











CSD87351Q5D

SLPS287E - MARCH 2011 - REVISED FEBRUARY 2017

CSD87351Q5D Synchronous Buck NexFET™ Power Block

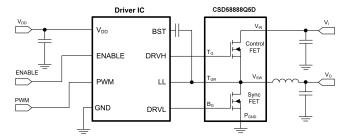
Features

- Half-Bridge Power Block
- 90% System Efficiency at 20 A
- Up to 32-A Operation
- High-Frequency Operation (up to 1.5 MHz)
- High-Density SON 5-mm x 6-mm Footprint
- Optimized for 5-V Gate Drive
- Low-Switching Losses
- Ultra-Low-Inductance Package
- **RoHS Compliant**
- Halogen Free
- Lead-Free Terminal Plating

Applications

- Synchronous Buck Converters
 - High-Frequency Applications
 - High-Current, Low-Duty Cycle Applications
- Multiphase Synchronous Buck Converters
- POL DC-DC Converters
- IMVP, VRM, and VRD Applications

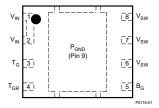
Typical Circuit



3 Description

The CSD87351Q5D NexFET™ power block is an optimized design for synchronous buck applications offering high-current, high-efficiency, and highfrequency capability in a small 5-mm × 6-mm outline. Optimized for 5-V gate drive applications, this product offers a flexible solution capable of offering a highdensity power supply when paired with any 5-V gate drive from an external controller/driver.

Top View



Device Information⁽¹⁾

DEVICE	MEDIA	QTY	PACKAGE	SHIP
CSD87351Q5D	13-Inch Reel	2500	SON 5.00-mm × 6.00-mm Plastic Package	Tape and Reel

(1) For all available packages, see the orderable addendum at the end of the data sheet.

Typical Power Block Efficiency and Power Loss

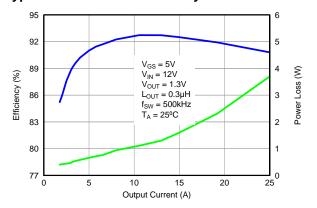




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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Chang	ges from Revision D (January 2012) to Revision E	Page
• Ad	dded note for I _{DM} in the <i>Absolute Maximum Ratings</i> table	3
• Ch	nanged part number in Figure 32	13
• Ad	dded the Device and Documentation Support section	17
Chang	ges from Revision C (October 2011) to Revision D	Page
• Ad	dded Feature Bullet: Up to 32 A Operation	1
Chang	ges from Revision B (September 2011) to Revision C	Page
• Ch	nanged "DIM a" Millimeter Max value From: 1.55 To: 1.5 and Inches Max value From: 0.061 To:	0.059 18
Chang	ges from Revision A (August 2011) to Revision B	Page
• Re	emove Z _{DS(on)} Max	4
• Re	emove Z _{DS(on)} Max	12
	dded Electrical Performance bullet	
Chang	ges from Original (March 2011) to Revision A	Page
• Re	eplaced R _{DS(on)} with Z _{DS(on)}	4
• Ad	dded Equivalent System Performance section	10

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5 Specifications

5.1 Absolute Maximum Ratings

 $T_A = 25$ °C (unless otherwise noted)⁽¹⁾

	PARAMETER	CONDITIONS	MIN	MAX	UNIT
		V _{IN} to P _{GND}	-0.8	30	
	Voltage	T_G to T_{GR}	-8	10	V
		B _G to P _{GND}	-8	10	
I _{DM} ⁽²⁾	Pulsed current rating	Pulsed current rating			
P _D	Power dissipation		12		W
_	Avalanaha anarav	Sync FET, $I_D = 87 \text{ A}$, $L = 0.1 \text{ mH}$	378	8	
E _{AS}	Avalanche energy	Avalanche energy Control FET, I _D = 44 A, L = 0.1 mH		•	mJ
TJ	Operating junction		-55	150	°C
T _{STG}	Storage temperature		-55	150	°C

⁽¹⁾ Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

5.2 Recommended Operating Conditions

 $T_A = 25^{\circ}C$ (unless otherwise noted)

	PARAMETER	CONDITIONS	MIN	MAX	UNIT
V_{GS}	Gate drive voltage		4.5	8	V
V_{IN}	Input supply voltage			27	V
$f_{\sf SW}$	Switching frequency	$C_{BST} = 0.1 \mu F (min)$	200	1500	kHz
	Operating current			32	Α
T _J	Operating temperature			125	°C

5.3 Power Block Performance

 $T_A = 25$ °C (unless otherwise noted)

	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
P _{LOSS} (1)	Power loss	$V_{IN} = 12 \text{ V, } V_{GS} = 5 \text{ V,}$ $V_{OUT} = 1.3 \text{ V, } I_{OUT} = 20 \text{ A,}$ $f_{SW} = 500 \text{ kHz,}$ $L_{OUT} = 0.3 \mu\text{H, } T_{J} = 25^{\circ}\text{C}$		2.5		W
I _{QVIN}	V _{IN} quiescent current	T_G to $T_{GR} = 0$ V B_G to $P_{GND} = 0$ V		10		μΑ

⁽¹⁾ Measurement made with six 10-µF (TDK C3216X5R1C106KT or equivalent) ceramic capacitors placed across V_{IN} to P_{GND} pins and using a high-current 5-V driver IC.

5.4 Thermal Information

 $T_A = 25$ °C (unless otherwise stated)

· A	(united states)				
	THERMAL METRIC	MIN	TYP	MAX	UNIT
В	Junction-to-ambient thermal resistance (min Cu) ⁽¹⁾⁽²⁾			119	°C/W
$R_{\theta JA}$	Junction-to-ambient thermal resistance (max Cu) ⁽¹⁾⁽²⁾			62	C/VV
В	Junction-to-case thermal resistance (top of package) (2)			25	°C/W
$R_{\theta JC}$	Junction-to-case thermal resistance (P _{GND} pin) ⁽²⁾			2.3	C/VV

⁽¹⁾ Device mounted on FR4 material with 1-in² (6.45-cm²) Cu.

⁽²⁾ Pulse duration \leq 50 µs. Duty cycle \leq 0.01%.

⁽²⁾ R_{BJC} is determined with the device mounted on a 1-in² (6.45-cm²), 2-oz (0.071-mm) thick Cu pad on a 1.5-in x 1.5-in (3.81-cm x 3.81-cm), 0.06-in (1.52-mm) thick FR4 board. R_{BJC} is specified by design while R_{BJA} is determined by the user's board design.

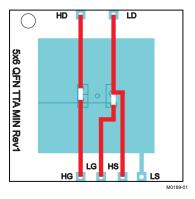


5.5 Electrical Characteristics

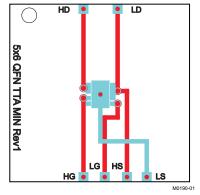
 $T_A = 25^{\circ}C$ (unless otherwise stated)

	DADAMETED	TEST COMPLETIONS	Q1 C	ontrol FE	ΕT		Q2 Sync FET			
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	MIN	TYP	MAX	UNIT	
STATIC CH	HARACTERISTICS				·			·		
BV _{DSS}	Drain-to-source voltage	$V_{GS} = 0 \text{ V}, I_{DS} = 250 \mu\text{A}$	30			30			V	
I _{DSS}	Drain-to-source leakage current	V _{GS} = 0 V, V _{DS} = 24 V			1			1	μΑ	
I _{GSS}	Gate-to-source leakage current	V _{DS} = 0 V, V _{GS} = +10 / -8			100			100	nA	
V _{GS(th)}	Gate-to-source threshold voltage	$V_{DS} = V_{GS}, I_{DS} = 250 \mu A$	1.0		2.1	0.75		1.15	V	
Z _{DS(on)} ⁽¹⁾	Effective AC on-impedance	$V_{IN} = 12 \text{ V}, V_{GS} = 5 \text{ V}, \ V_{OUT} = 1.3 \text{ V}, I_{OUT} = 20 \text{ A}, \ f_{SW} = 500 \text{ kHz}, \ L_{OUT} = 0.3 \mu\text{H}, \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$		7.4			1.6		mΩ	
9 _{fs}	Transconductance	$V_{DS} = 15 \text{ V}, I_{DS} = 20 \text{ A}$		75			142		S	
DYNAMIC	CHARACTERISTICS	-								
C _{ISS}	Input capacitance			966	1255		2410	3133	pF	
Coss	Output capacitance	$V_{GS} = 0 \text{ V}, V_{DS} = 15 \text{ V},$		382	497		1130	1469	pF	
C _{RSS}	Reverse transfer capacitance	f = 1 MHz		19	25		45	59	pF	
R _G	Series gate resistance			0.9	1.8		1	2	Ω	
Qg	Gate charge total (4.5 V)			5.9	7.7		17	22	nC	
Q _{gd}	Gate charge gate-to-drain	V _{DS} = 15 V,		1.1			3.1		nC	
Q _{gs}	Gate charge gate-to-source	I _{DS} = 20 A		2.1			3.7		nC	
Q _{g(th)}	Gate charge at Vth			1.1			2		nC	
Q _{OSS}	Output charge	$V_{DS} = 9.8 \text{ V}, V_{GS} = 0 \text{ V}$		6.5			23		nC	
t _{d(on)}	Turnon delay time			6.1			7.7		ns	
t _r	Rise time	$V_{DS} = 15 \text{ V}, V_{GS} = 4.5 \text{ V},$		16			10		ns	
t _{d(off)}	Turnoff delay time	$I_{DS} = 20 \text{ A}, R_G = 2 \Omega$		10			31		ns	
t _f	Fall time			2.1			4.2		ns	
DIODE CH	ARACTERISTICS	<u> </u>			,					
V_{SD}	Diode forward voltage	$I_{DS} = 20 \text{ A}, V_{GS} = 0 \text{ V}$		0.86	1		0.78	1	V	
Q _{rr}	Reverse recovery charge	$V_{dd} = 9.8 \text{ V}, I_F = 20 \text{ A},$		8.6			23		nC	
t _{rr}	Reverse recovery time	di/dt = 300 A/μs		16			24		ns	

(1) Equivalent system performance based on application testing. See Application and Implementation details.



Max $R_{\theta JA} = 62^{\circ} C/W$ when mounted on 1 in² (6.45 cm²) of 2-oz (0.071-mm) thick Cu.



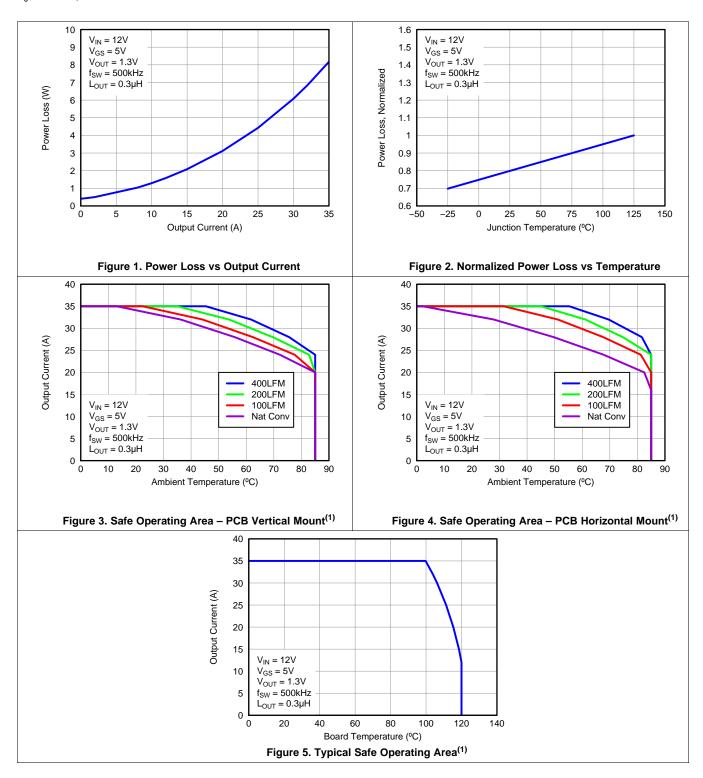
Max $R_{\theta JA} = 119^{\circ} C/W$ when mounted on minimum pad area of 2-oz (0.071-mm) thick Cu.

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5.6 Typical Power Block Device Characteristics

 $T_J = 125$ °C, unless stated otherwise

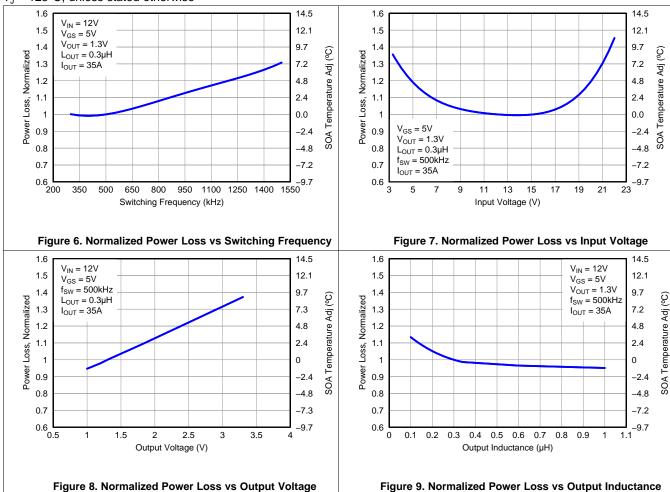


(1) The typical power block system characteristic curves are based on measurements made on a PCB design with dimensions of 4 in (W) × 3.5 in (L) × 0.062 in (H) and 6 copper layers of 1-oz copper thickness. See *Application and Implementation* for detailed explanation.



Typical Power Block Device Characteristics (continued)

 $T_J = 125$ °C, unless stated otherwise

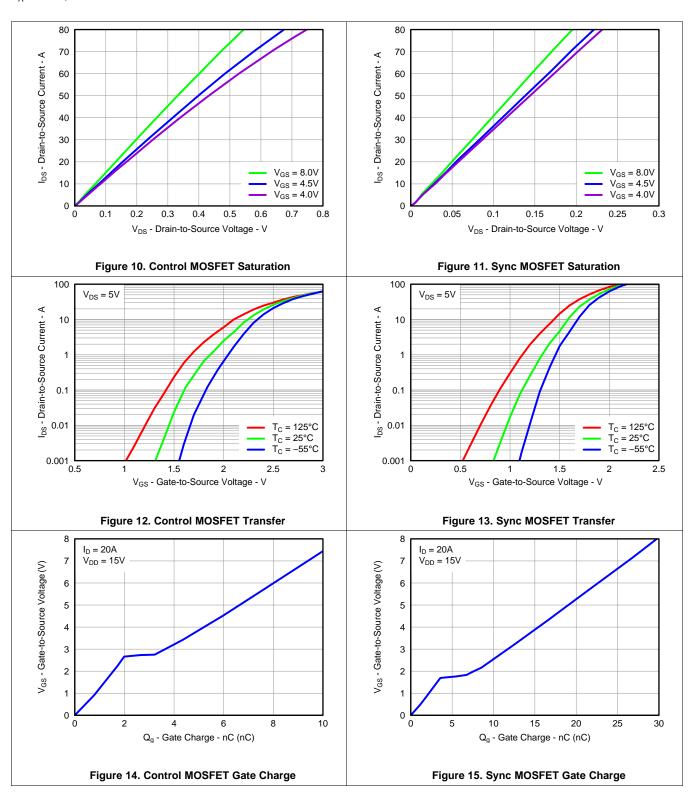


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5.7 Typical Power Block MOSFET Characteristics

 $T_A = 25$ °C, unless stated otherwise





Typical Power Block MOSFET Characteristics (continued)

 $T_A = 25$ °C, unless stated otherwise

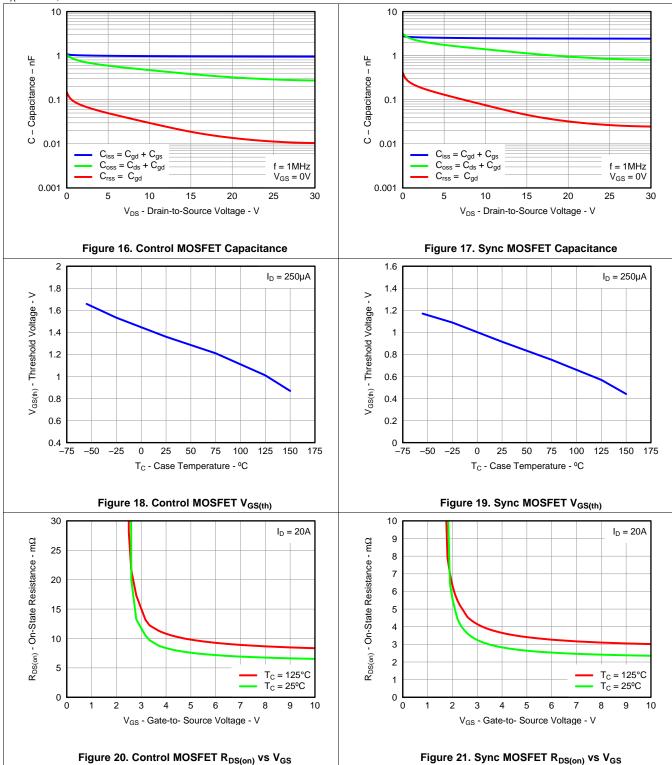
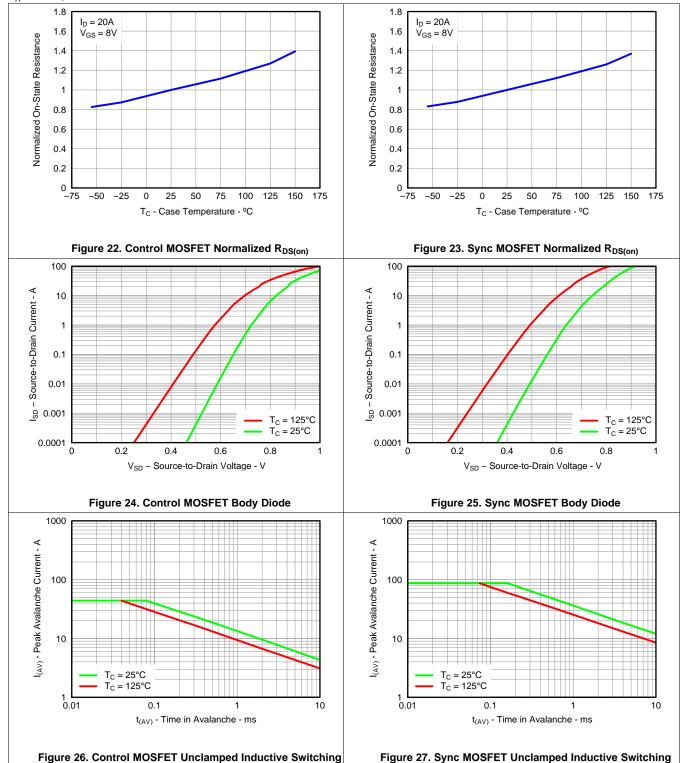


Figure 21. Sync MOSFET $R_{DS(on)}$ vs V_{GS}



Typical Power Block MOSFET Characteristics (continued)

 $T_A = 25$ °C, unless stated otherwise



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6 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

6.1 Application Information

6.1.1 Equivalent System Performance

Many of today's high-performance computing systems require low-power consumption in an effort to reduce system operating temperatures and improve overall system efficiency. This has created a major emphasis on improving the conversion efficiency of today's synchronous buck topology. In particular, there has been an emphasis in improving the performance of the critical power semiconductor in the power stage of this application (see Figure 28). As such, optimization of the power semiconductors in these applications, needs to go beyond simply reducing $R_{\rm DS(ON)}$.

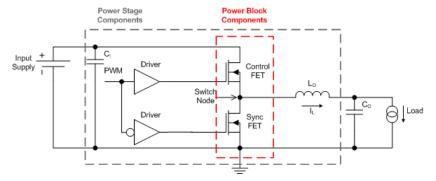


Figure 28. Equivalent System Schematic

The CSD87351Q5D is part of Tl's power block product family which is a highly optimized product for use in a synchronous buck topology requiring high current, high efficiency, and high frequency. It incorporates Tl's latest generation silicon which has been optimized for switching performance, as well as minimizing losses associated with $Q_{\rm GD}$, $Q_{\rm GS}$, and $Q_{\rm RR}$. Furthermore, Tl's patented packaging technology has minimized losses by nearly eliminating parasitic elements between the control FET and sync FET connections (see Figure 29). A key challenge solved by Tl's patented packaging technology is the system level impact of Common Source Inductance (CSI). CSI greatly impedes the switching characteristics of any MOSFET which in turn increases switching losses and reduces system efficiency. As a result, the effects of CSI need to be considered during the MOSFET selection process. In addition, standard MOSFET switching loss equations used to predict system efficiency need to be modified in order to account for the effects of CSI. Further details behind the effects of CSI and modification of switching loss equations are outlined in *Power Loss Calculation With Common Source Inductance Consideration for Synchronous Buck Converters* (SLPA009).

Product Folder Links: CSD87351Q5D

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Application Information (continued)

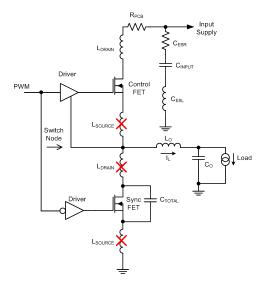
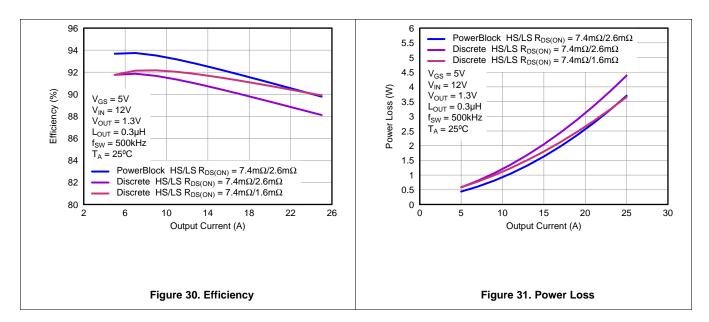


Figure 29. Elimination of Parasitic Inductances

The combination of TI's latest generation silicon and optimized packaging technology has created a bench marking solution that outperforms industry standard MOSFET chipsets of similar $R_{DS(ON)}$ and MOSFET chipsets with lower $R_{DS(ON)}$. Figure 30 and Figure 31 compare the efficiency and power loss performance of the CSD87351Q5D versus industry standard MOSFET chipsets commonly used in this type of application. This comparison purely focuses on the efficiency and generated loss of the power semiconductors only. The performance of CSD87351Q5D clearly highlights the importance of considering the effective AC on-impedance $(Z_{DS(ON)})$ during the MOSFET selection process of any new design. Simply normalizing to traditional MOSFET $R_{DS(ON)}$ specifications is not an indicator of the actual in-circuit performance when using TI's power block technology.



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Application Information (continued)

The chart below compares the traditional DC measured $R_{\rm DS(ON)}$ of CSD87351Q5D versus its $Z_{\rm DS(ON)}$. This comparison takes into account the improved efficiency associated with TI's patented packaging technology. As such, when comparing TI's power block products to individually packaged discrete MOSFETs or dual MOSFETs in a standard package, the in-circuit switching performance of the solution must be considered. In this example, individually packaged discrete MOSFETs or dual MOSFETs in a standard package would need to have DC measured $R_{\rm DS(ON)}$ values that are equivalent to CSD87351Q5D's $Z_{\rm DS(ON)}$ value in order to have the same efficiency performance at full load. Mid to light-load efficiency will still be lower with individually packaged discrete MOSFETs or dual MOSFETs in a standard package.

Table 1. Comparison of $R_{DS(ON)}$ vs $Z_{DS(ON)}$

PARAMETER	н	s	LS		
PARAMETER	TYP	MAX	TYP	MAX	
Effective AC on-impedance Z _{DS(ON)} (V _{GS} = 5 V)	7.4	-	1.6	-	
DC measured R _{DS(ON)} (V _{GS} = 4.5 V)	7.4	8.8	2.6	3.1	

The CSD87351Q5D NexFET™ power block is an optimized design for synchronous buck applications using 5-V gate drive. The control FET and sync FET silicon are parametrically tuned to yield the lowest power loss and highest system efficiency. As a result, a new rating method is needed which is tailored towards a more systemscentric environment. System-level performance curves such as power loss, Safe Operating Area (SOA), and normalized graphs allow engineers to predict the product performance in the actual application.

6.1.2 Power Loss Curves

MOSFET centric parameters such as $R_{DS(ON)}$ and Q_{gd} are needed to estimate the loss generated by the devices. In an effort to simplify the design process for engineers, Texas Instruments has provided measured power loss performance curves. Figure 1 plots the power loss of the CSD87351Q5D as a function of load current. This curve is measured by configuring and running the CSD87351Q5D as it would be in the final application (see Figure 32). The measured power loss is the CSD87351Q5D loss and consists of both input conversion loss and gate drive loss. Equation 1 is used to generate the power loss curve.

Power loss =
$$(V_{IN} \times I_{IN}) + (V_{DD} \times I_{DD}) - (V_{SW AVG} \times I_{OUT})$$
 (1)

The power loss curve in Figure 1 is measured at the maximum recommended junction temperatures of 125°C under isothermal test conditions.

6.1.3 Safe Operating Area (SOA) Curves

The SOA curves in the CSD87351Q5D data sheet provides guidance on the temperature boundaries within an operating system by incorporating the thermal resistance and system power loss. Figure 3 to Figure 5 outline the temperature and airflow conditions required for a given load current. The area under the curve dictates the safe operating area. All the curves are based on measurements made on a PCB design with dimensions of 4 in (W) \times 3.5 in (L) \times 0.062 in (T) and 6 copper layers of 1-oz copper thickness.

6.1.4 Normalized Curves

The normalized curves in the CSD87351Q5D data sheet provides guidance on the power loss and SOA adjustments based on their application specific needs. These curves show how the power loss and SOA boundaries will adjust for a given set of systems conditions. The primary Y-axis is the normalized change in power loss and the secondary Y-axis is the change is system temperature required in order to comply with the SOA curve. The change in power loss is a multiplier for the power loss curve and the change in temperature is subtracted from the SOA curve.



6.2 Typical Application

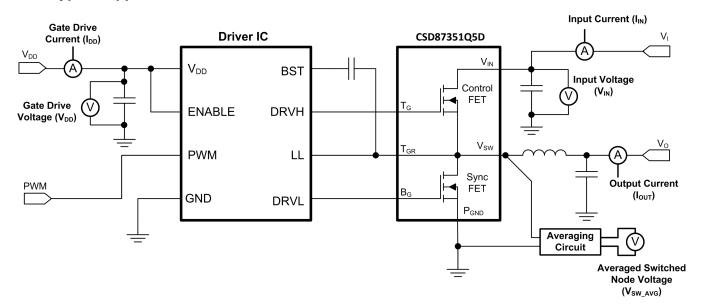


Figure 32. Typical Application

6.2.1 Calculating Power Loss and SOA

The user can estimate product loss and SOA boundaries by arithmetic means (see *Design Example*). Though the power loss and SOA curves in this data sheet are taken for a specific set of test conditions, the following procedure will outline the steps the user should take to predict product performance for any set of system conditions.

6.2.1.1 Design Example

Operating conditions:

- Output current = 25 A
- Input voltage = 7 V
- Output voltage = 1 V
- Switching frequency = 800 kHz
- Inductor = 0.2 μH

6.2.1.2 Calculating Power Loss

- Power loss at 25 A = 3.5 W (Figure 1)
- Normalized power loss for input voltage ≈ 1.07 (Figure 7)
- Normalized power loss for output voltage ≈ 0.95 (Figure 8)
- Normalized power loss for switching frequency ≈ 1.11 (Figure 6)
- Normalized power loss for output inductor ≈ 1.07 (Figure 9)
- Final calculated power loss = 3.5 W x 1.07 x 0.95 x 1.11 x 1.07 ≈ 4.23 W

6.2.1.3 Calculating SOA Adjustments

- SOA adjustment for input voltage ≈ 2°C (Figure 7)
- SOA adjustment for output voltage ≈ -1.3°C (Figure 8)
- SOA adjustment for switching frequency ≈ 2.8°C (Figure 6)
- SOA adjustment for output inductor ≈ 1.6°C (Figure 9)
- Final calculated SOA adjustment = 2 + (-1.3) + 2.8 + 1.6 ≈ 5.1°C

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Typical Application (continued)

In the design example above, the estimated power loss of the CSD87351Q5D would increase to 4.23 W. In addition, the maximum allowable board and/or ambient temperature would have to decrease by 5.1°C. Figure 33 graphically shows how the SOA curve would be adjusted accordingly.

- 1. Start by drawing a horizontal line from the application current to the SOA curve.
- 2. Draw a vertical line from the SOA curve intercept down to the board/ambient temperature.
- 3. Adjust the SOA board/ambient temperature by subtracting the temperature adjustment value.

In the design example, the SOA temperature adjustment yields a reduction in allowable board/ambient temperature of 5.1°C. In the event the adjustment value is a negative number, subtracting the negative number would yield an increase in allowable board/ambient temperature.

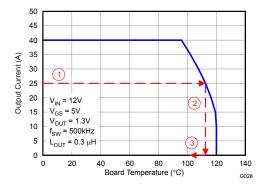


Figure 33. Power Block SOA

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7 Layout

7.1 Layout Guidelines

There are two key system-level parameters that can be addressed with a proper PCB design: electrical and thermal performance. Properly optimizing the PCB layout will yield maximum performance in both areas. A brief description on how to address each parameter is provided.

7.1.1 Electrical Performance

The power block has the ability to switch voltages at rates greater than 10 kV/µs. Special care must be then taken with the PCB layout design and placement of the input capacitors, driver IC, and output inductor.

- The placement of the input capacitors relative to the power block's VIN and PGND pins should have the highest priority during the component placement routine. It is critical to minimize these node lengths. As such, ceramic input capacitors need to be placed as close as possible to the VIN and PGND pins (see Figure 34). The example in Figure 34 uses 6, 10-µF ceramic capacitors (TDK part # C3216X5R1C106KT or equivalent). Notice there are ceramic capacitors on both sides of the board with an appropriate amount of vias interconnecting both layers. In terms of priority of placement next to the power block, C5, C7, C19, and C8 should follow in order.
- The driver IC should be placed relatively close to the power block gate pins. T_G and B_G should connect to the
 outputs of the driver IC. The T_{GR} pin serves as the return path of the high-side gate drive circuitry and should
 be connected to the phase pin of the IC (sometimes called LX, LL, SW, PH, etc.). The bootstrap capacitor for
 the driver IC will also connect to this pin.
- The switching node of the output inductor should be placed relatively close to the power block VSW pins. Minimizing the node length between these two components will reduce the PCB conduction losses and actually reduce the switching noise level.
- The switching node of the output inductor should be placed relatively close to the power block VSW pins. Minimizing the node length between these two components will reduce the PCB conduction losses and actually reduce the switching noise level. In the event the switch node waveform exhibits ringing that reaches undesirable levels, the use of a boost resistor or RC snubber can be an effective way to reduce the peak ring level. The recommended boost resistor value will range between 1 Ω to 4.7 Ω depending on the output characteristics of driver IC used in conjunction with the power block. The RC snubber values can range from 0.5 Ω to 2.2 Ω for the R and 330 pF to 2200 pF for the C. Refer to *Snubber Circuits: Theory*, *Design and Application* (SLUP100) for more details on how to properly tune the RC snubber values. The RC snubber should be placed as close as possible to the Vsw node and PGND see Figure 34. (1)

7.1.2 Thermal Performance

The power block has the ability to utilize the GND planes as the primary thermal path. As such, the use of thermal vias is an effective way to pull away heat from the device and into the system board. Concerns of solder voids and manufacturability problems can be addressed by the use of three basic tactics to minimize the amount of solder attach that will wick down the via barrel:

- Intentionally space out the vias from each other to avoid a cluster of holes in a given area.
- Use the smallest drill size allowed in your design. The example in Figure 34 uses vias with a 10-mil drill hole and a 16-mil capture pad.
- Tent the opposite side of the via with solder-mask.

In the end, the number and drill size of the thermal vias should align with the end user's PCB design rules and manufacturing capabilities.

 Keong W. Kam, David Pommerenke, "EMI Analysis Methods for Synchronous Buck Converter EMI Root Cause Analysis", University of Missouri – Rolla



7.2 Layout Example

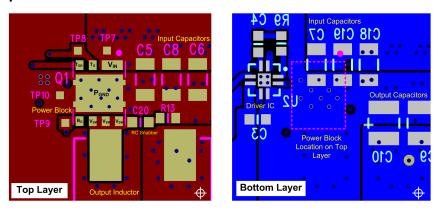


Figure 34. Recommended PCB Layout (Top Down View)



8 Device and Documentation Support

8.1 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

8.2 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

TI E2E™ Online Community TI's Engineer-to-Engineer (E2E) Community. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

Design Support *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

8.3 Trademarks

NexFET, E2E are trademarks of Texas Instruments.

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8.4 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

8.5 Glossary

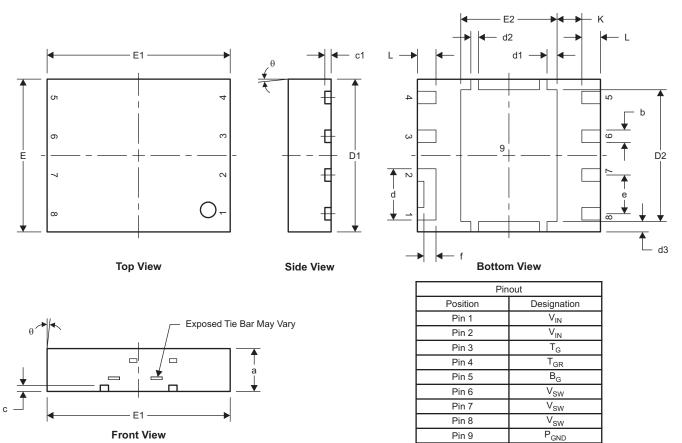
SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.



9 Mechanical, Packaging, and Orderable Information

9.1 Q5D Package Dimensions



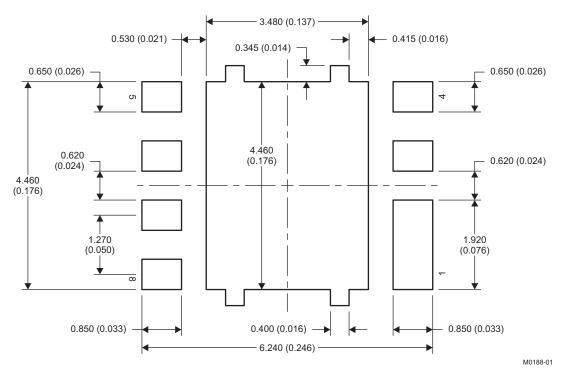
M	0	1	8	7	-	С

D.114	MILLIMETERS		INCHES	
DIM	MIN	MAX	MIN	MAX
а	1.400	1.500	0.055	0.059
b	0.360	0.460	0.014	0.018
С	0.150	0.250	0.006	0.010
c1	0.150	0.250	0.006	0.010
d	1.630	1.730	0.064	0.068
d1	0.280	0.380	0.011	0.015
d2	0.200	0.300	0.008	0.012
d3	0.291	0.391	0.012	0.015
D1	4.900	5.100	0.193	0.201
D2	4.269	4.369	0.168	0.172
Е	4.900	5.100	0.193	0.201
E1	5.900	6.100	0.232	0.240
E2	3.106	3.206	0.122	0.126
е	1.270 TYP		0.050	
f	0.396	0.496	0.016	0.020
L	0.510	0.710	0.020	0.028
θ	0.000	_	_	_
K	0.812		0.032	

Submit Documentation Feedback

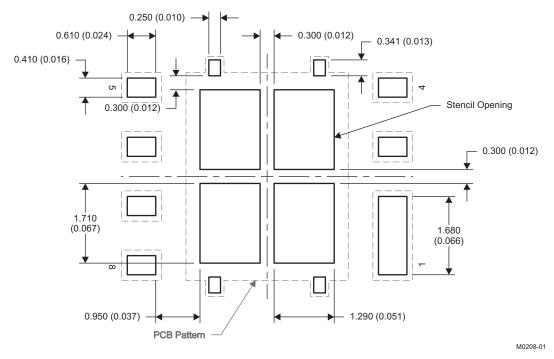


9.2 Land Pattern Recommendation



NOTE: Dimensions are in mm (in).

9.3 Stencil Recommendation

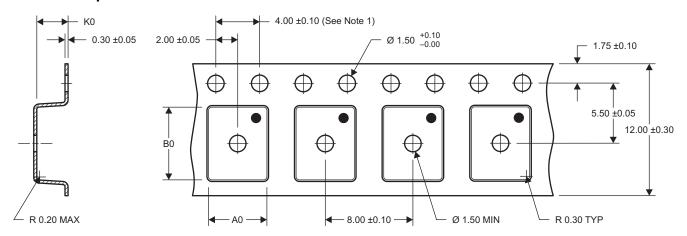


NOTE: Dimensions are in mm (in).

For recommended circuit layout for PCB designs, see *Reducing Ringing Through PCB Layout Techniques* (SLPA005).



9.4 Q5D Tape and Reel Information



A0 = 5.30 ±0.10 B0 = 6.50 ±0.10 K0 = 1.90 ±0.10

M0191-01

- NOTES: 1. 10-sprocket hole-pitch cumulative tolerance ±0.2.
 - 2. Camber not to exceed 1 mm in 100 mm, noncumulative over 250 mm.
 - 3. Material: black static-dissipative polystyrene.
 - 4. All dimensions are in mm, unless otherwise specified.
 - 5. Thickness: 0.3 ±0.05 mm.
 - 6. MSL1 260°C (IR and convection) PbF reflow compatible.

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PACKAGE OPTION ADDENDUM

3-Feb-2017

PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking	Samples
CSD87351Q5D	ACTIVE	LSON-CLIP	DQY	8		Pb-Free (RoHS Exempt)	CU NIPDAU CU SN	Level-1-260C-UNLIM	-55 to 150	87351D	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free** (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

- (3) MSL, Peak Temp. The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead/Ball Finish Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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3-Feb-2017

PACKAGE MATERIALS INFORMATION

www.ti.com 26-Apr-2017

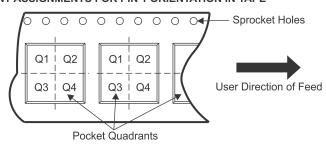
TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing			Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
CSD87351Q5D	LSON- CLIP	DQY	8	2500	330.0	15.4	5.3	6.3	1.2	8.0	12.0	Q2

www.ti.com 26-Apr-2017



*All dimensions are nominal

ĺ	Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)	
	CSD87351Q5D	LSON-CLIP	DQY	8	2500	335.0	335.0	32.0	

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